

# Standard Test Method for Conducting Erosion Tests by Solid Particle Impingement Using Gas Jets<sup>1</sup>

This standard is issued under the fixed designation G 76; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

# 1. Scope

1.1 This test method covers the determination of material loss by gas-entrained solid particle impingement erosion with jetnozzle type erosion equipment. This test method may be used in the laboratory to measure the solid particle erosion of different materials and has been used as a screening test for ranking solid particle erosion rates of materials in simulated service environments (1, 2).<sup>2</sup> Actual erosion service involves particle sizes, velocities, attack angles, environments, and so forth, that will vary over a wide range (3-5). Hence, any single laboratory test may not be sufficient to evaluate expected service performance. This test method describes one well characterized procedure for solid particle impingement erosion measurement for which interlaboratory test results are available.

1.2 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

# 2. Referenced Documents

2.1 ASTM Standards: <sup>3</sup>

E 122 Practice for Calculating Sample Size to Estimate, With a Specified Tolerable Error, the Average for a Characteristic of a Lot or Process

G 40 Terminology Relating to Wear and Erosion

2.2 American National Standard:

ANSI B74.10 Grading of Abrasive Microgrits<sup>4</sup>

## 3. Terminology

#### 3.1 *Definitions*:

3.1.1 *erosion*—progressive loss of original material from a solid surface due to mechanical interaction between that surface and a fluid, a multicomponent fluid, or impinging liquid or solid particles.

3.1.2 *impingement*—a process resulting in a continuing succession of impacts between (liquid or solid) particles and a solid surface.

3.2 Definitions of Terms Specific to This Standard:

3.2.1 *erosion value*—the volume loss of specimen material divided by the total mass of abrasive particles that impacted the specimen  $(mm^3 \cdot g^{-1})$ .

3.2.2 Normalized Erosion Rate—erosion value  $(mm^3 \cdot g^{-1})$  of specimen material divided by erosion value  $(mm^3 \cdot g^{-1})$  of reference material.

#### 4. Summary of Practice

4.1 This test method utilizes a repeated impact erosion approach involving a small nozzle delivering a stream of gas containing abrasive particles which impacts the surface of a test specimen. A standard set of test conditions is described. However, deviations from some of the standard conditions are permitted if described thoroughly. This allows for laboratory scale erosion measurements under a range of conditions. Test methods are described for preparing the specimens, conducting the erosion exposure, and reporting the results.

#### 5. Significance and Use

5.1 The significance of this test method in any overall measurements program to assess the erosion behavior of materials will depend on many factors concerning the conditions of service applications. The users of this test method should determine the degree of correlation of the results obtained with those from field performance or results using other test systems and methods. This test method may be used to rank the erosion resistance of materials under the specified conditions of testing.

Copyright © ASTM International, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959, United States.

<sup>&</sup>lt;sup>1</sup> This practice is under the jurisdiction of ASTM Committee G02 on Wear and Erosion and is the direct responsibility of Subcommittee G02.10 on Erosion by Solids and Liquids.

Current edition approved Jan. 1, 2004. Published January 2004. Originally approved in 1983. Last previous edition approved in 2002 as G 76 – 02.

<sup>&</sup>lt;sup>2</sup> Boldface numbers in parentheses refer to references at the end of this test method.

<sup>&</sup>lt;sup>3</sup> For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's Document Summary page on the ASTM website.

<sup>&</sup>lt;sup>4</sup> Available from American National Standards Institute (ANSI), 25 W. 43rd St., 4th Floor, New York, NY 10036.

# 6. Apparatus

6.1 The apparatus is capable of eroding material from a test specimen under well controlled exposure conditions. A schematic drawing of the exit nozzle and the particle-gas supply system is shown in Fig. 1. Deviations from this design are



FIG. 1 Schematic Drawing of Solid Particle Erosion Equipment

TABLE 1 Characteristics of Type 1020 Steel Reference Material

Annealed 15 min at 760°C (1400°F), air cooled.						
Hardness: HRB = 70 $\pm$ 2.						
Chemical Composition: $C = 0.20 \pm 0.01$ wt % $Mn = 0.45 \pm 0.10$ $S = 0.03 \pm 0.01$ $Si = 0.1 \pm 0.05$ $P = 0.01 \pm 0.01$						

permitted; however, adequate system characterization and control of critical parameters are required. Deviations in nozzle design and dimensions must be documented. Nozzle length to diameter ratio should be 25:1 or greater in order to achieve an acceptable particle velocity distribution in the stream. The recommended nozzle<sup>5</sup> consists of a tube about 1.5 mm inner diameter, 50 mm long, manufactured from an erosion resistant material such as WC,  $A1_2O_3$ , and so forth. Erosion of the nozzle during service shall be monitored and shall not exceed 10 % increase in the initial diameter.

6.2 Necessary features of the apparatus shall include a means of controlling and adjusting the particle impact velocity, particle flux, and the specimen location and orientation relative to the impinging stream.

6.3 Various means can be provided for introducing particles into the gas stream, including a vibrator-controlled hopper or a screw-feed system. It is required that the system provide a uniform particle feed and that it be adjustable to accommodate desired particle flow values.

6.4 A method to measure the particle velocity shall be available for use with the erosion equipment. Examples of accepted methods are high-speed photography (6), rotating double-disk (7), and laser velocimeter (8). Particle velocity shall be measured at the location to be occupied by the specimen and under the conditions of the test.

# 7. Test Materials and Sampling

7.1 This test method can be used over a range of specimen sizes and configurations. One convenient specimen configuration is a rectangular strip approximately 10 by 30 by 2 mm thick. Larger specimens and other shapes can be used where necessary, but must be documented.

7.2 The abrasive material to be used shall be uniform in essential characteristics such as particle size, moisture, chemical composition, and so forth.

7.3 Sampling of material for the purpose of obtaining representative test specimens shall be done in accordance with acceptable statistical practice. Practice E 122 shall be consulted.

## 8. Calibration of Apparatus

8.1 Specimens fabricated from Type 1020 steel (see Table 1 and Fig. 2) equivalent to that used in the interlaboratory test



FIG. 2 Microstructure of 1020 Steel Reference Material ASTM Grain Size 9

series<sup>6</sup> shall be tested periodically using specified (see Section 9) 50  $\mu$ m A1<sub>2</sub>O<sub>3</sub> particles to verify the satisfactory performance of the apparatus. It is recommended that performance be verified using this reference material every 50 tests during a measurement series, and also at the beginning of each new test series whenever the apparatus has been idle for some time. The recommended composition, heat treatment, and hardness range for this steel are listed in Table 1. The use of a steel of different composition may lead to different erosion results. A photomicrograph of the specified A1<sub>2</sub>O<sub>3</sub> particles is shown in Fig. 3.

<sup>&</sup>lt;sup>5</sup> A source for the recommended nozzle (tungsten carbide) is Kennametal, Inc., Latrobe, PA.

<sup>&</sup>lt;sup>6</sup> Supporting data have been filed at ASTM International Headquarters and may be obtained by requesting Research Report RR: G02–1003.



FIG. 3 Photomicrograph of 50 µm A1<sub>2</sub>O<sub>3</sub> Particles Used in Interlaboratory Testing

The range of erosion results to be expected for this steel under the standard test conditions specified in Section 9 is shown in Table 2 and is based on interlaboratory test results.<sup>6</sup>

8.2 Calibration at standard test conditions is recommended even if the apparatus is operated at other test conditions.

8.3 In any test program the particle velocity and particle feed rate shall be measured at frequent intervals, typically every ten tests, to ensure constancy of conditions.

## 9. Standard Test Conditions

9.1 This test method defines the following standard conditions.

9.1.1 The nozzle tube shall be 1.5 mm  $\pm$  0.075 mm inner diameter at least 50 mm long.

9.1.2 The test gas shall be dry air,  $-50^{\circ}$ C dew point or lower.

9.1.3 The abrasive particles shall be nominal 50- $\mu$ m angular A1<sub>2</sub>O<sub>3</sub>,<sup>7</sup> equivalent to those used in the interlaboratory test series (see Fig. 3). Abrasive shall be used only once.

9.1.4 The abrasive particle velocity shall be  $30 \pm 2 \text{ m} \cdot \text{s}^{-1}$ , measured at the specimen location. At this velocity the gas flow

<sup>7</sup> Aluminum oxide particles obtained from Norton Co., Worcester, MA as grade 240-grit alundum powder. Typical size distribution (determined by sedimentation): 100 % between 20 to 83 μm, 50 % between 42 to 57 μm, 50 % coarser than 48 μm.

ABLE 2	Interlaboratory	Test	Results	(Provisional)	۱
	menusoratory	1000	iteouto i	(i i o vi si o i u i j	,

Test Conditions	Laboratory Number	Number of Replicates	Average (.001 mm <sup>3</sup> /g)	Standard Deviation (.001 mm <sup>3</sup> /g)	Deviation from Average (.001 mm <sup>3</sup> /g)
Condition A:	1	9	2.240	0.420	-0.494
1020 steel,	2	9	3.130	0.130	0.396
50 µm Al <sub>2</sub> O <sub>3</sub> ,	3	10	2.130	0.068	-0.604
30 m/s, 90°	4	10	3.720	0.680	0.986
2 g/min	5	10	2.450	0.660	-0.284
	5	9.600	2.734	0.468	0.807
	Number	Average	Average	Within-Laboratory	Between-Laboratory
				Standard Deviation	Standard Deviation
			Coefficient of Variation (%) -	17 1	29.5
			95 % Limits -	1 31	2 26
			55 % Eimis =	Within-Laboratory	Between-Laboratory
Condition B <sup>1</sup>	1	8	31 500	1 100	3 340
1020 steel.	2	8	23.200	0.040	-4.960
50 µm Al <sub>2</sub> O <sub>2</sub> .	3	8	22.900	0.900	-5.260
70 m/s. 90°	4	4	32.400	0.650	4.240
2 g/min	5	8	30.800	1.500	2.640
	5	7.200	28.160	0.969	4.786
	Number	Average	Average	Within-Laboratory	Between-Laboratory
		Ū	C C	Standard Deviation	Standard Deviation
					(Provisional)
			Coefficient of Variation (%) =	3.4	17.0
			95 % Limits =	2.71	13.40
				Within-Laboratory	Between-Laboratory
Condition C:	1	8	40.000	1.300	7.640
304 stainless steel,	2	8	25.400	0.120	-6.960
50 µm Al <sub>2</sub> O <sub>3</sub> ,	3	8	26.300	0.780	-6.060
70 m/s, 90°	4	4	38.000	1.200	5.640
2 g/min	5	8	32.100	3.000	-0.260
	5	7.200	32.360	1.597	6.786
	Number	Average	Average	Within-Laboratory	Between-Laboratory
				Standard Deviation	Standard Deviation
					(Provisional)
			Coefficient of Variation (%) =	4.9	21.0
			95 % Limits =	4.47	19.00
				Within-Laboratory	Between-Laboratory

rate will be approximately 8  $\text{L}\cdot\text{min}^{-1}$  and the system pressure will be approximately 140 kPa (20 psig) although the pressure will depend on the specific system design.

9.1.5 The test time shall be 10 min to achieve steady state conditions. Longer times are permissible so long as the final erosion crater is no deeper than 1 mm.

9.1.6 The angle between the nozzle axis and the specimen surface shall be 90  $\pm$  2°.

9.1.7 The test temperature shall be the normal ambient value (typically between  $18^{\circ}$ C to  $28^{\circ}$ C).

9.1.8 The particle feed rate shall be  $2.0 \pm 0.5 \text{ g}\cdot\text{min}^{-1}$ . This corresponds to a particle flux at the specimen surface of about 2 mg·mm<sup>-2</sup>·s<sup>-1</sup> under standard conditions. Particle flux determination requires measurement of the eroded area on the specimen and is subject to considerable error. A measured width and depth profile of an erosion crater produced using stated conditions is shown in Fig. 4 and indicates a typical



FIG. 4 Example of Erosion Crater Profile for 1020 Steel Eroded at 70 m/s Particle Velocity Using Standard Conditions Otherwise

eroded width/depth relation.

9.1.9 The distance from specimen surface to nozzle end shall be 10  $\pm$  1 mm.

#### **10. Optional Test Conditions**

10.1 When test conditions or materials other than those given in Section 9 are used, reference to this test method shall clearly specify all test conditions and materials. It should be noted that other conditions, for example, larger particle velocities, may adversely affect measurement precision.

## **11. Test Procedure**

11.1 Establish and measure the particle velocity and particle flow specified. Adjust equipment controls to obtain proper velocity and flow conditions before inserting test specimens. Particle flow rate values are determined by collecting<sup>8</sup> and subsequently weighing the abrasive exiting from the nozzle for a measured time period.

11.2 Prepare the specimen surface if required to achieve uniformity and adequate finish. Grinding through a series of abrasive papers to 400 grit is usually adequate so long as all surface scale is removed. A surface roughness of 1  $\mu$ m (40  $\mu$ in.) rms or smaller is recommended. Clean the specimen surface carefully.<sup>9</sup> Weigh on an analytical balance to  $\pm 0.01$  mg.<sup>10</sup>

11.3 Mount the specimen in proper location and orientation in the apparatus. Subject the specimen to particle impingement for a selected time interval, measured to an accuracy of 5 s. Remove the specimen, clean carefully,<sup>9</sup> reweigh and calculate the mass loss.

11.4 Repeat this process to determine at least four points for a total time of at least 10 min and plot those values as mass loss versus elapsed time. Suitable times would be 2, 4, 8, and 16 min for a material such as Type 1020 steel. Steady state erosion should result after 1 to 2 min, depending on the material. Two examples of measured erosion versus time curves are shown in Fig. 5.



FIG. 5 Two Examples of Erosion versus Time for Type 1020 Steel at 30  $m \cdot s^{-1}$  and 70  $m \cdot s^{-1}$ 

11.5 The steady state erosion rate (see Terminology G 40) is determined from the slope of the mass loss versus time plot. The average erosion value is calculated by dividing erosion rate (mg·min<sup>-1</sup>) by the abrasive flow rate (g·min<sup>-1</sup>) and then dividing by the specimen density (g·cm<sup>-3</sup>). Report the average erosion value as (mm<sup>3</sup>·g<sup>-1</sup>).

11.6 Repeat 11.1 at the end of a series of tests (typically every 10 tests) and more frequently if necessary.

<sup>&</sup>lt;sup>8</sup> Particles may be collected by directing the flow from the nozzle into a large vented container. Care must be taken to avoid causing any significant back pressure on the nozzle as this will disturb the system flow conditions.

<sup>&</sup>lt;sup>9</sup> Important considerations in cleaning include surface oils or greases, surface rust or corrosion, adhering abrasive particles, etc.

 $<sup>^{10}</sup>$  Erosion weight loss determinations to ±0.1 mg may be sufficient for particle velocities above 70 m s $^{-1}$  or sufficiently long exposure times which lead to weight losses greater than 10 mg.

# 12. Report

12.1 The test report shall include the following information:

12.1.1 Material identification: type, chemical specification, heat and processing treatment, hardness, and density. Processing conditions shall include method of casting (such as chill or sand); method of forming (such as forging or pressing and sintering); and the percent of ideal density (important for ceramics and powder metallurgy alloys).

12.1.2 Specimens: method of preparing and cleaning specimens, initial surface roughness, and number tested.

12.1.3 Eroding particle identification: size distribution, shape, composition, purity, source, and manufacturing method. Provide photograph of typical collection of particles. Reference (9) can be consulted for information on methods of characterization.

12.1.4 Test conditions: particle velocity (average) and method of determination, specimen orientation relative to the impinging stream, particle flow, particle flux, eroded area (size, shape), temperature of the specimen and particles and carrier gas, test duration, method of determining steady-state erosion conditions, carrier gas composition, and method of determining the mass of abrasive used.

12.1.5 Description of the test equipment.

12.1.6 Tabulation of erosion value and standard deviation for each specimen reported as a volume loss of material per unit mass of abrasive (mm<sup>3</sup>·g<sup>-1</sup>).

12.2 Each test program shall include among the materials tested a reference material tested under the same conditions to permit calculation and report of the normalized erosion rate. A suitable reference material would be Type 1020 steel (see Table 1).

12.3 The report shall state clearly whether testing was done at standard conditions, shall itemize any deviations from those conditions, and shall indicate the frequency of calibration using reference materials. 12.4 Any special occurrences or observations during testing should be noted.

#### 13. Precision and Bias

13.1 Absolute values of erosion rates of materials are generally not available because of the wide range of possible exposure conditions. The erosion measurement conditions established by this practice are designed to facilitate obtaining precise, reproducible data applicable to the test conditions employed. Interlaboratory test results utilizing this practice on well-characterized metal are given in Table 2. Examples of 95 % confidence limits for three erosion test conditions are shown in Table 2. For Condition A, a statement of precision would be: average erosion was  $2.73 \times 10^{-3}$  mm <sup>3</sup>/g; 95 % repeatability limit was  $1.31 \times 10^{-3}$  mm<sup>3</sup>/g; 95 % reproducibility limit was  $2.26 \times 10^{-3}$  mm<sup>3</sup>/g.

13.2 No bias can be assigned to this test method since there is no absolute accepted value for erosion rate.

13.3 General Considerations—Participants in the interlaboratory testing that led to the statements of precision and bias given above involve five laboratories, two different materials, two test conditions, and five replicate measurements each. Subsequent to this testing, described in Research Report # G02–1003 that is available from ASTM, data were received from another laboratory that utilized a commercial test machine. Those data were found consistent with the results of the interlaboratory study and will be included in the research report.

#### 14. Keywords

14.1 erosion; erosion rate; gas jet; metal erosion; solid particle

#### REFERENCES

- (1) Young, J. P., and Ruff, A. W., *Journal of Engineering Materials and Technology, Transactions of ASME*, Vol 99, 1977, pp. 121–125.
- (2) Hansen, J. S., in *Erosion: Prevention and Useful Applications*, Adler, W. F., ed., ASTM STP 664, 1979, pp. 148–162.
- (3) Finnie, I., Levy, A., and McFadden, D. H., in *Erosion: Prevention and Useful Applications*, Adler, W. F., ed., *ASTM STP 664*, 1979, pp. 36–58.
- (4) Wood, F.W., Journal of Testing and Evaluation, 14, 1986.
- (5) Preece, C. M., ed., *Erosion: Treatise on Materials Science and Technology*, Vol 16 Academic Press, New York, NY, 1979.
- (6) Finnie, I., Wolak, J., and Kabil, Y., *Journal of Materials*, Vol 2, 1967, pp. 682–700.
- (7) Ninham, A.J., and Hutchins, I.M., Proceedings of the 6th International Conference on Erosion by Liquid and Solid Impact (Univ. of Cambridge, 1983) pp. 50-51.
- (8) Barkalow, R. H., Goebel, J. A., and Pettit, F. S., in *Erosion: Prevention and Useful Applications*, Adler, W. F., ed., *ASTM STP 664*, 1979, pp. 163–192.
- (9) Allen, T., Particle Size Measurement, Chapman and Hall, London, 1974.
- (10) Ponnaganti, V., Stock, D.E., and Sheldon, G.L., Proceedings on Symposium Polyphase Flow and Transport Tech. (ASME) NY, 1980 pp 195-199.

ASTM International takes no position respecting the validity of any patent rights asserted in connection with any item mentioned in this standard. Users of this standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, are entirely their own responsibility.

This standard is subject to revision at any time by the responsible technical committee and must be reviewed every five years and if not revised, either reapproved or withdrawn. Your comments are invited either for revision of this standard or for additional standards and should be addressed to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee, which you may attend. If you feel that your comments have not received a fair hearing you should make your views known to the ASTM Committee on Standards, at the address shown below.

This standard is copyrighted by ASTM International, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959, United States. Individual reprints (single or multiple copies) of this standard may be obtained by contacting ASTM at the above address or at 610-832-9585 (phone), 610-832-9555 (fax), or service@astm.org (e-mail); or through the ASTM website (www.astm.org).